

# GRAZ Engineering, L.L.C.



323 West Lake Road • Fitzwilliam, NH 03447 • Telephone (603) 585-6959 • Fax (603) 585-6960

## Transmittal

**To:** Conservation Commission

**Company:** Town of Leicester

**Address:** 3 Washburn Square

**City/State:** Leicester, MA 01524

**Subject:** Revised Oak Bluff Lane  
Definitive Plans

**Date:** March 7, 2019

**Transmitted:** ☐ Mail ☐ Fax ☒ Hand

- ☒ For Your Approval
- ☒ For Your Review
- ☐ For Your Signature
- ☒ For Your Information
- ☐ For Your Files

- ☒ Which You requested
- ☐ Approved
- ☐ Approved As Noted
- ☐ Revise And Resubmit
- ☐ Not Approved

1	copies	DEP Oak Bluff Lane Definitive Subdivision Revision Letter dated 3/7/19
1	copies	Revised Oak Bluff Lane Definitive Subdivision Plans dated 3/5/19 (Full Size Plans)
2	copies	Revised Stormwater & Hydrology & Stormwater Documents dated 3/5/19
1	CD	Revised PDF Digital Copy of Submittal Materials dated 3/5/19
	copies	
	copies	
	copies	
	copies	
	copies	

**Comments:** Enclosed are the revised plans and associated documentation for the Oak Bluff Lane Definitive Subdivision located off from Baldwin Street.

Should you have any questions or require any additional information, please call my cell at 508-769-9084.

Respectfully yours,  
GRAZ Engineering, L.L.C.

Brian MacEwen, P.L.S., E.I.T.  
Project Manager

cc: Matt Schold, Applicant/Owner

# GRAZ Engineering, L.L.C.



323 West Lake Road • Fitzwilliam, NH 03447 • Telephone (603) 585-6959 • Fax (603) 585-6960

March 7, 2019

Judith Schmitz  
Massachusetts DEP  
8 New Bond Street  
Worcester, MA 01606

**Subject: Oak Bluff Lane  
Definitive Subdivision Revision 1**

Dear Ms. Schmitz:

GRAZ Engineering, L.L.C. (GRAZ) has received and reviewed your email comments dated January 9, 2019 regarding the proposed Oak Bluff Lane Definitive Subdivision to be located off Baldwin Street dated.

On behalf of Central Land Development Corp. (Matt Schold) and in response to your comments and the subsequent comments received during the Leicester Planning Board (LPB) and Leicester Conservation Commission public hearings to date, GRAZ submits the following item-by-item responses and the revised subdivision plans and associated documentation for your files.

## **DEP Comments:**

*Isolated vegetated wetlands B and C should be shown on the site plans if they are located within the footprint of the proposed project. Although these areas may not be jurisdictional under the Massachusetts Wetlands Protection Act, filling of isolated vegetated wetlands may require 401 Water Quality Certification.*

**The isolated wetlands B and C are not located within the footprint of this proposed project and are not impacted by the work proposed under this project and therefore it is not necessary to depict these wetlands on plans. These isolated wetlands are located approximately 470-feet to the west of the nearest point of this proposed project near the easterly side of Lake Avenue in Spencer.**

*Construction of the stormwater basins (southern stormwater basin and forebay, and northern forebay) that intercept groundwater is not recommended since maintaining the capacity of these basins relies on a functioning subdrain..*

**Pond (#54P) adjacent to the wetlands along Baldwin Street was designed as wet detention pond with no allowance for infiltration due to the groundwater table elevation. As originally designed, the sediment forebay (#55P) is designed to provide a groundwater separation of  $\pm 2.4$ -feet (proposed basin bottom = 866.8 versus groundwater elevation of 864.4). This forebay and pond have been maintained as originally designed due to that existing site topography, the proximity of the adjacent wetlands, and in an effort to minimize site grading while maintaining the existing footprint/alignment of the existing gravel road for the proposed roadway alignment.**

**The northern pond (#71P) and its associated sediment forebay have been revised to provide  $\pm 2.8$ -feet of separation from the estimated seasonal high groundwater table elevation at the critical upgradient side of the basin. This provides sufficient separation from the groundwater table accounting for the groundwater mounding at that location due to the basin (see mounding analysis).**

*Will the Basin 71P subdrain interfere with the infiltration functions of the basin? The inspection, evaluation and potential replacement of the detention basin subdrains is not included in the O & M plan. In addition, the subdrains may not contribute to draining the basins after storm events during period of high groundwater.*

**The subdrains in Basins 54P and 71P are designed strictly for maintenance drawdown and as such have been designed with a shut-off valve.**

*Recharge calculations provided to meet Stormwater Standard 3 do not include the presence of groundwater intercepting the Basin 70P forebay, nor are mounding calculations provided for either basin. Calculations are not provided to demonstrate that Basin 54P drains within 72 hours of a storm event.*

**The recharge calculations for Basin 70P forebay have been revised to reflect the proposed grading that provide  $\pm 2.8$ -feet of groundwater separation as required by the standard.**

*Subcatchments 30 and 31 do not fully meet Stormwater Standard 4. Can additional BMPs be provided to fully comply with the Massachusetts Stormwater Standards?*

**Due to the existing site topography, the proximity of the adjacent wetlands, and in an effort to minimize site grading while maintaining the existing footprint/alignment of the existing gravel road for the proposed roadway alignment other than the pea gravel stone diaphragm along the westerly edge of the roadway entrance, the proposed grassed swale with check dams, and the sediment forebay (55P), there are no other additional BMP's that could be feasibly or economically cited at this location to provide full compliance with the Standards.**

I trust that this information clarifies the comments that you had relative to the original subdivision submittal. Should you have any other questions or require additional information please email me as soon as possible.

Respectfully yours,

GRAZ Engineering, L.L.C.

  
Brian MacEwen, P.L.S., E.I.T.  
Project Manager

  
Paul Grasewicz, P.E., P.L.S.

BCM/PFG/bcm

cc: Matt Schold, Central Land Development Corp.  
Paul Grasewicz, GRAZ Engineering, LLC

<b>TABLE OF PRE AND POST TOTAL FLOWS FOR ANALYSIS POINTS OF 2, 10, 25, &amp; 100 YR STORMS (CFS)</b>				
	<i>2</i>	<i>10</i>	<i>25</i>	<i>100</i>
<i>PRE (1P)</i>	<i>6.53</i>	<i>15.36</i>	<i>20.59</i>	<i>30.54</i>
<i>POST (50P)</i>	<i>6.49</i>	<i>14.95</i>	<i>20.51</i>	<i>29.23</i>
<i>PRE (3S)</i>	<i>7.32</i>	<i>17.99</i>	<i>24.37</i>	<i>34.42</i>
<i>POST (72P)</i>	<i>6.83</i>	<i>17.43</i>	<i>24.18</i>	<i>34.23</i>
<i>PRE (4S)</i>	<i>0.64</i>	<i>1.62</i>	<i>2.21</i>	<i>3.14</i>
<i>POST (41S)</i>	<i>0.51</i>	<i>1.35</i>	<i>1.85</i>	<i>2.65</i>
<i>PRE (5S)</i>	<i>0.13</i>	<i>0.34</i>	<i>0.46</i>	<i>0.66</i>
<i>POST (34S)</i>	<i>0.12</i>	<i>0.32</i>	<i>0.44</i>	<i>0.63</i>

**Post-Development***Type III 24-hr 2 yr Rainfall=3.00"*

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Time span=1.00-24.00 hrs, dt=0.01 hrs, 2301 points  
 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
 Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

**Subcatchment 43S: Subcatchment 43** Runoff Area=25,261 sf 0.00% Impervious Runoff Depth>1.19"  
 Flow Length=244' Tc=5.0 min CN=79 Runoff=0.82 cfs 2,499 cf

**Subcatchment 44S: Subcatchment 44** Runoff Area=406,918 sf 6.01% Impervious Runoff Depth>0.85"  
 Flow Length=811' Slope=0.0650 '/ S Tc=13.0 min CN=73 Runoff=6.83 cfs 28,967 cf

**Pond 69P: DMH6** Peak Elev=873.66' Inflow=1.85 cfs 5,633 cf  
 15.0" Round Culvert n=0.012 L=156.2' S=0.0109 '/ Outflow=1.85 cfs 5,633 cf

**Pond 70P: Sediment Forebay 70P** Peak Elev=870.75' Storage=750 cf Inflow=1.85 cfs 5,633 cf  
 Discarded=0.00 cfs 265 cf Primary=1.79 cfs 4,795 cf Secondary=0.00 cfs 0 cf Outflow=1.79 cfs 5,060 cf

**Pond 71P: Infiltration Basin 71P** Peak Elev=870.29' Storage=3,636 cf Inflow=2.60 cfs 7,294 cf  
 Discarded=0.02 cfs 899 cf Primary=0.24 cfs 3,767 cf Secondary=0.00 cfs 0 cf Outflow=0.26 cfs 4,666 cf

**Pond 72P: Stiles Lake** Inflow=6.83 cfs 32,733 cf  
 Primary=6.83 cfs 32,733 cf

**Pond 73P: DMH7** Peak Elev=871.92' Inflow=1.85 cfs 5,633 cf  
 15.0" Round Culvert n=0.012 L=9.6' S=0.0104 '/ Outflow=1.85 cfs 5,633 cf

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**Summary for Subcatchment 43S: Subcatchment 43**

Runoff = 0.82 cfs @ 12.08 hrs, Volume= 2,499 cf, Depth&gt; 1.19"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs  
Type III 24-hr 2 yr Rainfall=3.00"

Area (sf)	CN	Description
5,424	96	Gravel surface, HSG C
19,837	74	>75% Grass cover, Good, HSG C
25,261	79	Weighted Average
25,261		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0	244		0.81		Direct Entry,

**Summary for Subcatchment 44S: Subcatchment 44**

Runoff = 6.83 cfs @ 12.20 hrs, Volume= 28,967 cf, Depth&gt; 0.85"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs  
Type III 24-hr 2 yr Rainfall=3.00"

Area (sf)	CN	Description
* 24,436	98	Pavement & Roofs, HSG C
3,694	96	Gravel surface, HSG C
75,817	74	>75% Grass cover, Good, HSG C
5,317	80	>75% Grass cover, Good, HSG D
297,654	70	Woods, Good, HSG C
406,918	73	Weighted Average
382,482		93.99% Pervious Area
24,436		6.01% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
13.0	811	0.0650	1.04		Lag/CN Method,

**Summary for Pond 69P: DMH6**

Inflow Area = 43,070 sf, 43.75% Impervious, Inflow Depth > 1.57" for 2 yr event  
 Inflow = 1.85 cfs @ 12.08 hrs, Volume= 5,633 cf  
 Outflow = 1.85 cfs @ 12.08 hrs, Volume= 5,633 cf, Atten= 0%, Lag= 0.0 min  
 Primary = 1.85 cfs @ 12.08 hrs, Volume= 5,633 cf

Routing by Dyn-Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs  
 Peak Elev= 873.66' @ 12.08 hrs  
 Flood Elev= 876.40'

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Device	Routing	Invert	Outlet Devices
#1	Primary	872.90'	<b>15.0" Round Culvert</b> L= 156.2' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 872.90' / 871.20' S= 0.0109 '/' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf

**Primary OutFlow** Max=1.84 cfs @ 12.08 hrs HW=873.66' TW=871.92' (Dynamic Tailwater)

↑ **1=Culvert** (Inlet Controls 1.84 cfs @ 2.35 fps)

### Summary for Pond 70P: Sediment Forebay 70P

Inflow Area = 43,070 sf, 43.75% Impervious, Inflow Depth > 1.57" for 2 yr event  
 Inflow = 1.85 cfs @ 12.08 hrs, Volume= 5,633 cf  
 Outflow = 1.79 cfs @ 12.09 hrs, Volume= 5,060 cf, Atten= 3%, Lag= 1.1 min  
 Discarded = 0.00 cfs @ 12.09 hrs, Volume= 265 cf  
 Primary = 1.79 cfs @ 12.09 hrs, Volume= 4,795 cf  
 Secondary = 0.00 cfs @ 1.00 hrs, Volume= 0 cf

Routing by Dyn-Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

Peak Elev= 870.75' @ 12.09 hrs Surf.Area= 776 sf Storage= 750 cf

Flood Elev= 873.30' Surf.Area= 1,522 sf Storage= 3,302 cf

Plug-Flow detention time= 72.3 min calculated for 5,060 cf (90% of inflow)

Center-of-Mass det. time= 22.9 min ( 843.8 - 820.9 )

Volume	Invert	Avail.Storage	Storage Description
#1	869.50'	3,302 cf	<b>Custom Stage Data (Prismatic)</b> Listed below (Recalc)
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
869.50	435	0	0
870.00	559	249	249
871.00	848	704	952
872.00	1,165	1,007	1,959
873.00	1,522	1,344	3,302

Device	Routing	Invert	Outlet Devices
#1	Primary	870.50'	<b>143.1 deg x 4.0' long x 1.50' rise Sharp-Crested Vee/Trap Weir</b> Cv= 2.47 (C= 3.09)
#2	Secondary	872.00'	<b>12.0' long x 1.0' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31 3.30 3.31 3.32
#3	Discarded	869.50'	<b>0.270 in/hr Exfiltration over Surface area</b>

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**Discarded OutFlow** Max=0.00 cfs @ 12.09 hrs HW=870.75' (Free Discharge)↑ **3=Exfiltration** (Exfiltration Controls 0.00 cfs)**Primary OutFlow** Max=1.78 cfs @ 12.09 hrs HW=870.75' TW=869.63' (Dynamic Tailwater)↑ **1=Sharp-Crested Vee/Trap Weir** (Weir Controls 1.78 cfs @ 1.50 fps)**Secondary OutFlow** Max=0.00 cfs @ 1.00 hrs HW=869.50' TW=868.50' (Dynamic Tailwater)↑ **2=Broad-Crested Rectangular Weir** (Controls 0.00 cfs)**Summary for Pond 71P: Infiltration Basin 71P**

Inflow Area = 68,331 sf, 27.58% Impervious, Inflow Depth > 1.28" for 2 yr event  
 Inflow = 2.60 cfs @ 12.09 hrs, Volume= 7,294 cf  
 Outflow = 0.26 cfs @ 13.04 hrs, Volume= 4,666 cf, Atten= 90%, Lag= 57.2 min  
 Discarded = 0.02 cfs @ 13.04 hrs, Volume= 899 cf  
 Primary = 0.24 cfs @ 13.04 hrs, Volume= 3,767 cf  
 Secondary = 0.00 cfs @ 1.00 hrs, Volume= 0 cf

Routing by Dyn-Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

Peak Elev= 870.29' @ 13.04 hrs Surf.Area= 3,411 sf Storage= 3,636 cf

Flood Elev= 873.30' Surf.Area= 11,664 sf Storage= 21,023 cf

Plug-Flow detention time= 233.8 min calculated for 4,664 cf (64% of inflow)

Center-of-Mass det. time= 130.4 min ( 972.3 - 842.0 )

Volume	Invert	Avail.Storage	Storage Description
#1	868.50'	21,023 cf	<b>Custom Stage Data (Prismatic)</b> Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
868.50	0	0	0
869.00	1,015	254	254
869.50	2,765	945	1,199
870.00	3,166	1,483	2,682
871.00	4,010	3,588	6,270
872.00	6,156	5,083	11,353
873.00	7,450	6,803	18,156
873.30	11,664	2,867	21,023

Device	Routing	Invert	Outlet Devices
#1	Primary	862.20'	<b>12.0" Round Culvert</b> L= 69.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 862.20' / 858.00' S= 0.0609 1' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#2	Device 1	869.80'	<b>30.0 deg x 1.30' rise Sharp-Crested Vee/Trap Weir X 2.00</b> Cv= 2.61 (C= 3.26)
#3	Device 1	871.60'	<b>1.2" x 7.3" Horiz. Orifice/Grate X 3.00 columns</b> X 11 rows C= 0.600 in 25.7" x 25.7" Grate (44% open area) Limited to weir flow at low heads
#4	Secondary	871.60'	<b>170.5 deg x 5.0' long x 1.00' rise Sharp-Crested Vee/Trap Weir</b>



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#5 Discarded 868.50'  $C_v = 2.46$  ( $C = 3.08$ ) **0.270 in/hr Exfiltration over Surface area**

**Discarded OutFlow** Max=0.02 cfs @ 13.04 hrs HW=870.29' (Free Discharge)↑ **5=Exfiltration** (Exfiltration Controls 0.02 cfs)**Primary OutFlow** Max=0.24 cfs @ 13.04 hrs HW=870.29' TW=0.00' (Dynamic Tailwater)↑ **1=Culvert** (Passes 0.24 cfs of 10.42 cfs potential flow)↑ **2=Sharp-Crested Vee/Trap Weir** (Weir Controls 0.24 cfs @ 1.83 fps)↑ **3=Orifice/Grate** (Controls 0.00 cfs)**Secondary OutFlow** Max=0.00 cfs @ 1.00 hrs HW=868.50' TW=0.00' (Dynamic Tailwater)↑ **4=Sharp-Crested Vee/Trap Weir** (Controls 0.00 cfs)**Summary for Pond 72P: Stiles Lake**

Inflow Area = 475,249 sf, 9.11% Impervious, Inflow Depth > 0.83" for 2 yr event  
 Inflow = 6.83 cfs @ 12.20 hrs, Volume= 32,733 cf  
 Primary = 6.83 cfs @ 12.20 hrs, Volume= 32,733 cf, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

**Summary for Pond 73P: DMH7**

Inflow Area = 43,070 sf, 43.75% Impervious, Inflow Depth > 1.57" for 2 yr event  
 Inflow = 1.85 cfs @ 12.08 hrs, Volume= 5,633 cf  
 Outflow = 1.85 cfs @ 12.08 hrs, Volume= 5,633 cf, Atten= 0%, Lag= 0.0 min  
 Primary = 1.85 cfs @ 12.08 hrs, Volume= 5,633 cf

Routing by Dyn-Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

Peak Elev= 871.92' @ 12.08 hrs

Flood Elev= 874.50'

Device	Routing	Invert	Outlet Devices
#1	Primary	871.10'	<b>15.0" Round Culvert</b> L= 9.6' CPP, projecting, no headwall, $K_e = 0.900$ Inlet / Outlet Invert= 871.10' / 871.00' $S = 0.0104$ ' / $C_c = 0.900$ $n = 0.012$ , Flow Area= 1.23 sf

**Primary OutFlow** Max=1.84 cfs @ 12.08 hrs HW=871.92' TW=870.75' (Dynamic Tailwater)↑ **1=Culvert** (Barrel Controls 1.84 cfs @ 3.06 fps)

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Type III 24-hr 10 yr Rainfall=4.50"

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Time span=1.00-24.00 hrs, dt=0.01 hrs, 2301 points  
 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
 Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

**Subcatchment 43S: Subcatchment 43** Runoff Area=25,261 sf 0.00% Impervious Runoff Depth>2.37"  
 Flow Length=244' Tc=5.0 min CN=79 Runoff=1.68 cfs 4,998 cf

**Subcatchment 44S: Subcatchment 44** Runoff Area=406,918 sf 6.01% Impervious Runoff Depth>1.89"  
 Flow Length=811' Slope=0.0650 '/' Tc=13.0 min CN=73 Runoff=16.28 cfs 64,087 cf

**Pond 69P: DMH6** Peak Elev=874.04' Inflow=3.36 cfs 10,249 cf  
 15.0" Round Culvert n=0.012 L=156.2' S=0.0109 '/' Outflow=3.36 cfs 10,249 cf

**Pond 70P: Sediment Forebay 70P** Peak Elev=870.86' Storage=838 cf Inflow=3.36 cfs 10,249 cf  
 Discarded=0.01 cfs 292 cf Primary=3.29 cfs 9,380 cf Secondary=0.00 cfs 0 cf Outflow=3.29 cfs 9,672 cf

**Pond 71P: Infiltration Basin 71P** Peak Elev=870.84' Storage=5,635 cf Inflow=4.94 cfs 14,377 cf  
 Discarded=0.02 cfs 987 cf Primary=1.54 cfs 10,560 cf Secondary=0.00 cfs 0 cf Outflow=1.56 cfs 11,547 cf

**Pond 72P: Stiles Lake** Inflow=17.43 cfs 74,647 cf  
 Primary=17.43 cfs 74,647 cf

**Pond 73P: DMH7** Peak Elev=872.30' Inflow=3.36 cfs 10,249 cf  
 15.0" Round Culvert n=0.012 L=9.6' S=0.0104 '/' Outflow=3.36 cfs 10,249 cf

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**Summary for Subcatchment 43S: Subcatchment 43**

Runoff = 1.68 cfs @ 12.08 hrs, Volume= 4,998 cf, Depth&gt; 2.37"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs  
Type III 24-hr 10 yr Rainfall=4.50"

Area (sf)	CN	Description
5,424	96	Gravel surface, HSG C
19,837	74	>75% Grass cover, Good, HSG C
25,261	79	Weighted Average
25,261		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0	244		0.81		Direct Entry,

**Summary for Subcatchment 44S: Subcatchment 44**

Runoff = 16.28 cfs @ 12.18 hrs, Volume= 64,087 cf, Depth&gt; 1.89"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs  
Type III 24-hr 10 yr Rainfall=4.50"

Area (sf)	CN	Description
* 24,436	98	Pavement & Roofs, HSG C
3,694	96	Gravel surface, HSG C
75,817	74	>75% Grass cover, Good, HSG C
5,317	80	>75% Grass cover, Good, HSG D
297,654	70	Woods, Good, HSG C
406,918	73	Weighted Average
382,482		93.99% Pervious Area
24,436		6.01% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
13.0	811	0.0650	1.04		Lag/CN Method,

**Summary for Pond 69P: DMH6**

Inflow Area = 43,070 sf, 43.75% Impervious, Inflow Depth > 2.86" for 10 yr event  
 Inflow = 3.36 cfs @ 12.07 hrs, Volume= 10,249 cf  
 Outflow = 3.36 cfs @ 12.07 hrs, Volume= 10,249 cf, Atten= 0%, Lag= 0.0 min  
 Primary = 3.36 cfs @ 12.07 hrs, Volume= 10,249 cf

Routing by Dyn-Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs  
 Peak Elev= 874.04' @ 12.07 hrs  
 Flood Elev= 876.40'

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Device	Routing	Invert	Outlet Devices
#1	Primary	872.90'	<b>15.0" Round Culvert</b> L= 156.2' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 872.90' / 871.20' S= 0.0109 '/' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf

**Primary OutFlow** Max=3.35 cfs @ 12.07 hrs HW=874.03' TW=872.30' (Dynamic Tailwater)

↑ **1=Culvert** (Inlet Controls 3.35 cfs @ 2.86 fps)

### Summary for Pond 70P: Sediment Forebay 70P

Inflow Area = 43,070 sf, 43.75% Impervious, Inflow Depth > 2.86" for 10 yr event  
 Inflow = 3.36 cfs @ 12.07 hrs, Volume= 10,249 cf  
 Outflow = 3.29 cfs @ 12.09 hrs, Volume= 9,672 cf, Atten= 2%, Lag= 0.9 min  
 Discarded = 0.01 cfs @ 12.09 hrs, Volume= 292 cf  
 Primary = 3.29 cfs @ 12.09 hrs, Volume= 9,380 cf  
 Secondary = 0.00 cfs @ 1.00 hrs, Volume= 0 cf

Routing by Dyn-Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

Peak Elev= 870.86' @ 12.09 hrs Surf.Area= 808 sf Storage= 838 cf

Flood Elev= 873.30' Surf.Area= 1,522 sf Storage= 3,302 cf

Plug-Flow detention time= 48.3 min calculated for 9,668 cf (94% of inflow)

Center-of-Mass det. time= 17.7 min ( 823.9 - 806.2 )

Volume	Invert	Avail.Storage	Storage Description
#1	869.50'	3,302 cf	<b>Custom Stage Data (Prismatic)</b> Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
869.50	435	0	0
870.00	559	249	249
871.00	848	704	952
872.00	1,165	1,007	1,959
873.00	1,522	1,344	3,302

Device	Routing	Invert	Outlet Devices
#1	Primary	870.50'	<b>143.1 deg x 4.0' long x 1.50' rise Sharp-Crested Vee/Trap Weir</b> Cv= 2.47 (C= 3.09)
#2	Secondary	872.00'	<b>12.0' long x 1.0' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31 3.30 3.31 3.32
#3	Discarded	869.50'	<b>0.270 in/hr Exfiltration over Surface area</b>

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**Discarded OutFlow** Max=0.01 cfs @ 12.09 hrs HW=870.86' (Free Discharge)↑ **3=Exfiltration** (Exfiltration Controls 0.01 cfs)**Primary OutFlow** Max=3.28 cfs @ 12.09 hrs HW=870.86' TW=870.43' (Dynamic Tailwater)↑ **1=Sharp-Crested Vee/Trap Weir** (Weir Controls 3.28 cfs @ 1.78 fps)**Secondary OutFlow** Max=0.00 cfs @ 1.00 hrs HW=869.50' TW=868.50' (Dynamic Tailwater)↑ **2=Broad-Crested Rectangular Weir** (Controls 0.00 cfs)**Summary for Pond 71P: Infiltration Basin 71P**

Inflow Area = 68,331 sf, 27.58% Impervious, Inflow Depth > 2.52" for 10 yr event  
 Inflow = 4.94 cfs @ 12.08 hrs, Volume= 14,377 cf  
 Outflow = 1.56 cfs @ 12.39 hrs, Volume= 11,547 cf, Atten= 68%, Lag= 18.6 min  
 Discarded = 0.02 cfs @ 12.39 hrs, Volume= 987 cf  
 Primary = 1.54 cfs @ 12.39 hrs, Volume= 10,560 cf  
 Secondary = 0.00 cfs @ 1.00 hrs, Volume= 0 cf

Routing by Dyn-Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

Peak Elev= 870.84' @ 12.39 hrs Surf.Area= 3,874 sf Storage= 5,635 cf

Flood Elev= 873.30' Surf.Area= 11,664 sf Storage= 21,023 cf

Plug-Flow detention time= 145.4 min calculated for 11,542 cf (80% of inflow)

Center-of-Mass det. time= 71.5 min ( 895.4 - 824.0 )

Volume	Invert	Avail.Storage	Storage Description
#1	868.50'	21,023 cf	<b>Custom Stage Data (Prismatic)</b> Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
868.50	0	0	0
869.00	1,015	254	254
869.50	2,765	945	1,199
870.00	3,166	1,483	2,682
871.00	4,010	3,588	6,270
872.00	6,156	5,083	11,353
873.00	7,450	6,803	18,156
873.30	11,664	2,867	21,023

Device	Routing	Invert	Outlet Devices
#1	Primary	862.20'	<b>12.0" Round Culvert</b> L= 69.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 862.20' / 858.00' S= 0.0609 1' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#2	Device 1	869.80'	<b>30.0 deg x 1.30' rise Sharp-Crested Vee/Trap Weir X 2.00</b> Cv= 2.61 (C= 3.26)
#3	Device 1	871.60'	<b>1.2" x 7.3" Horiz. Orifice/Grate X 3.00 columns</b> X 11 rows C= 0.600 in 25.7" x 25.7" Grate (44% open area) Limited to weir flow at low heads
#4	Secondary	871.60'	<b>170.5 deg x 5.0' long x 1.00' rise Sharp-Crested Vee/Trap Weir</b>

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Cv= 2.46 (C= 3.08)  
 #5 Discarded 868.50' **0.270 in/hr Exfiltration over Surface area**

**Discarded OutFlow** Max=0.02 cfs @ 12.39 hrs HW=870.84' (Free Discharge)↑**5=Exfiltration** (Exfiltration Controls 0.02 cfs)**Primary OutFlow** Max=1.54 cfs @ 12.39 hrs HW=870.84' TW=0.00' (Dynamic Tailwater)↑**1=Culvert** (Passes 1.54 cfs of 10.79 cfs potential flow)↑**2=Sharp-Crested Vee/Trap Weir** (Weir Controls 1.54 cfs @ 2.66 fps)↑**3=Orifice/Grate** ( Controls 0.00 cfs)**Secondary OutFlow** Max=0.00 cfs @ 1.00 hrs HW=868.50' TW=0.00' (Dynamic Tailwater)↑**4=Sharp-Crested Vee/Trap Weir** ( Controls 0.00 cfs)**Summary for Pond 72P: Stiles Lake**

Inflow Area = 475,249 sf, 9.11% Impervious, Inflow Depth > 1.88" for 10 yr event  
 Inflow = 17.43 cfs @ 12.19 hrs, Volume= 74,647 cf  
 Primary = 17.43 cfs @ 12.19 hrs, Volume= 74,647 cf, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

**Summary for Pond 73P: DMH7**

Inflow Area = 43,070 sf, 43.75% Impervious, Inflow Depth > 2.86" for 10 yr event  
 Inflow = 3.36 cfs @ 12.07 hrs, Volume= 10,249 cf  
 Outflow = 3.36 cfs @ 12.07 hrs, Volume= 10,249 cf, Atten= 0%, Lag= 0.0 min  
 Primary = 3.36 cfs @ 12.07 hrs, Volume= 10,249 cf

Routing by Dyn-Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

Peak Elev= 872.30' @ 12.07 hrs

Flood Elev= 874.50'

Device	Routing	Invert	Outlet Devices
#1	Primary	871.10'	<b>15.0" Round Culvert</b> L= 9.6' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 871.10' / 871.00' S= 0.0104 '/ Cc= 0.900 n= 0.012, Flow Area= 1.23 sf

**Primary OutFlow** Max=3.35 cfs @ 12.07 hrs HW=872.30' TW=870.86' (Dynamic Tailwater)↑**1=Culvert** (Barrel Controls 3.35 cfs @ 3.54 fps)

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*Type III 24-hr 25 yr Rainfall=5.30"*

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Time span=1.00-24.00 hrs, dt=0.01 hrs, 2301 points  
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

**Subcatchment 43S: Subcatchment 43** Runoff Area=25,261 sf 0.00% Impervious Runoff Depth>3.06"  
Flow Length=244' Tc=5.0 min CN=79 Runoff=2.16 cfs 6,439 cf

**Subcatchment 44S: Subcatchment 44** Runoff Area=406,918 sf 6.01% Impervious Runoff Depth>2.51"  
Flow Length=811' Slope=0.0650 '/' Tc=13.0 min CN=73 Runoff=21.88 cfs 85,143 cf

**Pond 69P: DMH6** Peak Elev=874.33' Inflow=4.19 cfs 12,840 cf  
15.0" Round Culvert n=0.012 L=156.2' S=0.0109 '/' Outflow=4.19 cfs 12,840 cf

**Pond 70P: Sediment Forebay 70P** Peak Elev=871.07' Storage=1,011 cf Inflow=4.19 cfs 12,840 cf  
Discarded=0.01 cfs 303 cf Primary=3.92 cfs 11,958 cf Secondary=0.00 cfs 0 cf Outflow=3.92 cfs 12,261 cf

**Pond 71P: Infiltration Basin 71P** Peak Elev=871.06' Storage=6,504 cf Inflow=6.08 cfs 18,397 cf  
Discarded=0.03 cfs 1,036 cf Primary=2.48 cfs 14,447 cf Secondary=0.00 cfs 0 cf Outflow=2.51 cfs 15,483 cf

**Pond 72P: Stiles Lake** Inflow=24.18 cfs 99,590 cf  
Primary=24.18 cfs 99,590 cf

**Pond 73P: DMH7** Peak Elev=872.53' Inflow=4.19 cfs 12,840 cf  
15.0" Round Culvert n=0.012 L=9.6' S=0.0104 '/' Outflow=4.19 cfs 12,840 cf

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**Summary for Subcatchment 43S: Subcatchment 43**

Runoff = 2.16 cfs @ 12.07 hrs, Volume= 6,439 cf, Depth&gt; 3.06"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs  
Type III 24-hr 25 yr Rainfall=5.30"

Area (sf)	CN	Description
5,424	96	Gravel surface, HSG C
19,837	74	>75% Grass cover, Good, HSG C
25,261	79	Weighted Average
25,261		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0	244		0.81		Direct Entry,

**Summary for Subcatchment 44S: Subcatchment 44**

Runoff = 21.88 cfs @ 12.18 hrs, Volume= 85,143 cf, Depth&gt; 2.51"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs  
Type III 24-hr 25 yr Rainfall=5.30"

Area (sf)	CN	Description
* 24,436	98	Pavement & Roofs, HSG C
3,694	96	Gravel surface, HSG C
75,817	74	>75% Grass cover, Good, HSG C
5,317	80	>75% Grass cover, Good, HSG D
297,654	70	Woods, Good, HSG C
406,918	73	Weighted Average
382,482		93.99% Pervious Area
24,436		6.01% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
13.0	811	0.0650	1.04		Lag/CN Method,

**Summary for Pond 69P: DMH6**

Inflow Area = 43,070 sf, 43.75% Impervious, Inflow Depth > 3.58" for 25 yr event  
 Inflow = 4.19 cfs @ 12.07 hrs, Volume= 12,840 cf  
 Outflow = 4.19 cfs @ 12.07 hrs, Volume= 12,840 cf, Atten= 0%, Lag= 0.0 min  
 Primary = 4.19 cfs @ 12.07 hrs, Volume= 12,840 cf

Routing by Dyn-Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs  
 Peak Elev= 874.33' @ 12.07 hrs  
 Flood Elev= 876.40'



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Device	Routing	Invert	Outlet Devices
#1	Primary	872.90'	<b>15.0" Round Culvert</b> L= 156.2' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 872.90' / 871.20' S= 0.0109 '/' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf

**Primary OutFlow** Max=4.18 cfs @ 12.07 hrs HW=874.33' TW=872.53' (Dynamic Tailwater)

↑**1=Culvert** (Inlet Controls 4.18 cfs @ 3.40 fps)

**Summary for Pond 70P: Sediment Forebay 70P**

Inflow Area = 43,070 sf, 43.75% Impervious, Inflow Depth > 3.58" for 25 yr event  
Inflow = 4.19 cfs @ 12.07 hrs, Volume= 12,840 cf  
Outflow = 3.92 cfs @ 12.08 hrs, Volume= 12,261 cf, Atten= 6%, Lag= 0.3 min  
Discarded = 0.01 cfs @ 12.29 hrs, Volume= 303 cf  
Primary = 3.92 cfs @ 12.08 hrs, Volume= 11,958 cf  
Secondary = 0.00 cfs @ 1.00 hrs, Volume= 0 cf

Routing by Dyn-Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

Peak Elev= 871.07' @ 12.29 hrs Surf.Area= 870 sf Storage= 1,011 cf

Flood Elev= 873.30' Surf.Area= 1,522 sf Storage= 3,302 cf

Plug-Flow detention time= 41.8 min calculated for 12,261 cf (95% of inflow)

Center-of-Mass det. time= 16.4 min ( 817.0 - 800.6 )

Volume	Invert	Avail.Storage	Storage Description
#1	869.50'	3,302 cf	<b>Custom Stage Data (Prismatic)</b> Listed below (Recalc)
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
869.50	435	0	0
870.00	559	249	249
871.00	848	704	952
872.00	1,165	1,007	1,959
873.00	1,522	1,344	3,302

Device	Routing	Invert	Outlet Devices
#1	Primary	870.50'	<b>143.1 deg x 4.0' long x 1.50' rise Sharp-Crested Vee/Trap Weir</b> Cv= 2.47 (C= 3.09)
#2	Secondary	872.00'	<b>12.0' long x 1.0' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31 3.30 3.31 3.32
#3	Discarded	869.50'	<b>0.270 in/hr Exfiltration over Surface area</b>

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**Discarded OutFlow** Max=0.01 cfs @ 12.29 hrs HW=871.07' (Free Discharge)↑ **3=Exfiltration** (Exfiltration Controls 0.01 cfs)**Primary OutFlow** Max=3.68 cfs @ 12.08 hrs HW=870.92' TW=870.74' (Dynamic Tailwater)↑ **1=Sharp-Crested Vee/Trap Weir** (Weir Controls 3.68 cfs @ 1.65 fps)**Secondary OutFlow** Max=0.00 cfs @ 1.00 hrs HW=869.50' TW=868.50' (Dynamic Tailwater)↑ **2=Broad-Crested Rectangular Weir** (Controls 0.00 cfs)**Summary for Pond 71P: Infiltration Basin 71P**

Inflow Area = 68,331 sf, 27.58% Impervious, Inflow Depth > 3.23" for 25 yr event  
 Inflow = 6.08 cfs @ 12.08 hrs, Volume= 18,397 cf  
 Outflow = 2.51 cfs @ 12.29 hrs, Volume= 15,483 cf, Atten= 59%, Lag= 13.1 min  
 Discarded = 0.03 cfs @ 12.29 hrs, Volume= 1,036 cf  
 Primary = 2.48 cfs @ 12.29 hrs, Volume= 14,447 cf  
 Secondary = 0.00 cfs @ 1.00 hrs, Volume= 0 cf

Routing by Dyn-Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

Peak Elev= 871.06' @ 12.29 hrs Surf.Area= 4,133 sf Storage= 6,504 cf

Flood Elev= 873.30' Surf.Area= 11,664 sf Storage= 21,023 cf

Plug-Flow detention time= 125.3 min calculated for 15,483 cf (84% of inflow)

Center-of-Mass det. time= 60.6 min ( 877.9 - 817.4 )

Volume	Invert	Avail.Storage	Storage Description
#1	868.50'	21,023 cf	<b>Custom Stage Data (Prismatic)</b> Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
868.50	0	0	0
869.00	1,015	254	254
869.50	2,765	945	1,199
870.00	3,166	1,483	2,682
871.00	4,010	3,588	6,270
872.00	6,156	5,083	11,353
873.00	7,450	6,803	18,156
873.30	11,664	2,867	21,023

Device	Routing	Invert	Outlet Devices
#1	Primary	862.20'	<b>12.0" Round Culvert</b> L= 69.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 862.20' / 858.00' S= 0.0609 1' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#2	Device 1	869.80'	<b>30.0 deg x 1.30' rise Sharp-Crested Vee/Trap Weir X 2.00</b> Cv= 2.61 (C= 3.26)
#3	Device 1	871.60'	<b>1.2" x 7.3" Horiz. Orifice/Grate X 3.00 columns</b> X 11 rows C= 0.600 in 25.7" x 25.7" Grate (44% open area) Limited to weir flow at low heads
#4	Secondary	871.60'	<b>170.5 deg x 5.0' long x 1.00' rise Sharp-Crested Vee/Trap Weir</b>

**Post-Development**



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
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Cv= 2.46 (C= 3.08)  
 #5 Discarded 868.50' **0.270 in/hr Exfiltration over Surface area**

**Discarded OutFlow** Max=0.03 cfs @ 12.29 hrs HW=871.06' (Free Discharge)

**5=Exfiltration** (Exfiltration Controls 0.03 cfs)
**Primary OutFlow** Max=2.48 cfs @ 12.29 hrs HW=871.06' TW=0.00' (Dynamic Tailwater)

**1=Culvert** (Passes 2.48 cfs of 10.93 cfs potential flow)


**2=Sharp-Crested Vee/Trap Weir** (Weir Controls 2.48 cfs @ 2.93 fps)


**3=Orifice/Grate** ( Controls 0.00 cfs)
**Secondary OutFlow** Max=0.00 cfs @ 1.00 hrs HW=868.50' TW=0.00' (Dynamic Tailwater)

**4=Sharp-Crested Vee/Trap Weir** ( Controls 0.00 cfs)
**Summary for Pond 72P: Stiles Lake**

Inflow Area = 475,249 sf, 9.11% Impervious, Inflow Depth > 2.51" for 25 yr event  
 Inflow = 24.18 cfs @ 12.18 hrs, Volume= 99,590 cf  
 Primary = 24.18 cfs @ 12.18 hrs, Volume= 99,590 cf, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

**Summary for Pond 73P: DMH7**


Inflow Area = 43,070 sf, 43.75% Impervious, Inflow Depth > 3.58" for 25 yr event  
 Inflow = 4.19 cfs @ 12.07 hrs, Volume= 12,840 cf  
 Outflow = 4.19 cfs @ 12.07 hrs, Volume= 12,840 cf, Atten= 0%, Lag= 0.0 min  
 Primary = 4.19 cfs @ 12.07 hrs, Volume= 12,840 cf

Routing by Dyn-Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

Peak Elev= 872.53' @ 12.07 hrs

Flood Elev= 874.50'

Device	Routing	Invert	Outlet Devices
#1	Primary	871.10'	<b>15.0" Round Culvert</b> L= 9.6' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 871.10' / 871.00' S= 0.0104 '/ Cc= 0.900 n= 0.012, Flow Area= 1.23 sf

**Primary OutFlow** Max=4.18 cfs @ 12.07 hrs HW=872.53' TW=870.92' (Dynamic Tailwater)

**1=Culvert** (Inlet Controls 4.18 cfs @ 3.40 fps)

**Post-Development***Type III 24-hr 100 yr Rainfall=6.50"*

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Time span=1.00-24.00 hrs, dt=0.01 hrs, 2301 points

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN

Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

**Subcatchment 43S: Subcatchment 43**Runoff Area=25,261 sf 0.00% Impervious Runoff Depth>4.13"  
Flow Length=244' Tc=5.0 min CN=79 Runoff=2.90 cfs 8,685 cf**Subcatchment 44S: Subcatchment 44**Runoff Area=406,918 sf 6.01% Impervious Runoff Depth>3.50"  
Flow Length=811' Slope=0.0650 '/' Tc=13.0 min CN=73 Runoff=30.69 cfs 118,636 cf**Pond 69P: DMH6**Peak Elev=874.89' Inflow=5.44 cfs 16,826 cf  
15.0" Round Culvert n=0.012 L=156.2' S=0.0109 '/' Outflow=5.44 cfs 16,826 cf**Pond 70P: Sediment Forebay 70P**Peak Elev=871.37' Storage=1,286 cf Inflow=5.44 cfs 16,826 cf  
Discarded=0.01 cfs 317 cf Primary=4.66 cfs 15,928 cf Secondary=0.00 cfs 0 cf Outflow=4.66 cfs 16,245 cf**Pond 71P: Infiltration Basin 71P**Peak Elev=871.36' Storage=7,855 cf Inflow=7.55 cfs 24,612 cf  
Discarded=0.03 cfs 1,109 cf Primary=3.60 cfs 20,483 cf Secondary=0.00 cfs 0 cf Outflow=3.63 cfs 21,592 cf**Pond 72P: Stiles Lake**Inflow=34.23 cfs 139,119 cf  
Primary=34.23 cfs 139,119 cf**Pond 73P: DMH7**Peak Elev=873.09' Inflow=5.44 cfs 16,826 cf  
15.0" Round Culvert n=0.012 L=9.6' S=0.0104 '/' Outflow=5.44 cfs 16,826 cf

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**Summary for Subcatchment 43S: Subcatchment 43**

Runoff = 2.90 cfs @ 12.07 hrs, Volume= 8,685 cf, Depth&gt; 4.13"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs  
Type III 24-hr 100 yr Rainfall=6.50"

Area (sf)	CN	Description
5,424	96	Gravel surface, HSG C
19,837	74	>75% Grass cover, Good, HSG C
25,261	79	Weighted Average
25,261		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0	244		0.81		Direct Entry,

**Summary for Subcatchment 44S: Subcatchment 44**

Runoff = 30.69 cfs @ 12.18 hrs, Volume= 118,636 cf, Depth&gt; 3.50"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs  
Type III 24-hr 100 yr Rainfall=6.50"

Area (sf)	CN	Description
* 24,436	98	Pavement & Roofs, HSG C
3,694	96	Gravel surface, HSG C
75,817	74	>75% Grass cover, Good, HSG C
5,317	80	>75% Grass cover, Good, HSG D
297,654	70	Woods, Good, HSG C
406,918	73	Weighted Average
382,482		93.99% Pervious Area
24,436		6.01% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
13.0	811	0.0650	1.04		Lag/CN Method,

**Summary for Pond 69P: DMH6**

Inflow Area = 43,070 sf, 43.75% Impervious, Inflow Depth > 4.69" for 100 yr event  
 Inflow = 5.44 cfs @ 12.07 hrs, Volume= 16,826 cf  
 Outflow = 5.44 cfs @ 12.07 hrs, Volume= 16,826 cf, Atten= 0%, Lag= 0.0 min  
 Primary = 5.44 cfs @ 12.07 hrs, Volume= 16,826 cf

Routing by Dyn-Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs  
 Peak Elev= 874.89' @ 12.07 hrs  
 Flood Elev= 876.40'

**Post-Development**

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Device	Routing	Invert	Outlet Devices
#1	Primary	872.90'	<b>15.0" Round Culvert</b> L= 156.2' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 872.90' / 871.20' S= 0.0109 '/' Cc= 0.900 n= 0.012, Flow Area= 1.23 sf

**Primary OutFlow** Max=5.43 cfs @ 12.07 hrs HW=874.88' TW=873.08' (Dynamic Tailwater)↑**1=Culvert** (Inlet Controls 5.43 cfs @ 4.43 fps)**Summary for Pond 70P: Sediment Forebay 70P**

Inflow Area = 43,070 sf, 43.75% Impervious, Inflow Depth > 4.69" for 100 yr event  
 Inflow = 5.44 cfs @ 12.07 hrs, Volume= 16,826 cf  
 Outflow = 4.66 cfs @ 12.08 hrs, Volume= 16,245 cf, Atten= 14%, Lag= 0.2 min  
 Discarded = 0.01 cfs @ 12.25 hrs, Volume= 317 cf  
 Primary = 4.66 cfs @ 12.08 hrs, Volume= 15,928 cf  
 Secondary = 0.00 cfs @ 1.00 hrs, Volume= 0 cf

Routing by Dyn-Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

Peak Elev= 871.37' @ 12.25 hrs Surf.Area= 965 sf Storage= 1,286 cf

Flood Elev= 873.30' Surf.Area= 1,522 sf Storage= 3,302 cf

Plug-Flow detention time= 35.1 min calculated for 16,238 cf (97% of inflow)

Center-of-Mass det. time= 15.0 min ( 808.9 - 793.8 )

Volume	Invert	Avail.Storage	Storage Description
#1	869.50'	3,302 cf	<b>Custom Stage Data (Prismatic)</b> Listed below (Recalc)
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
869.50	435	0	0
870.00	559	249	249
871.00	848	704	952
872.00	1,165	1,007	1,959
873.00	1,522	1,344	3,302

Device	Routing	Invert	Outlet Devices
#1	Primary	870.50'	<b>143.1 deg x 4.0' long x 1.50' rise Sharp-Crested Vee/Trap Weir</b> Cv= 2.47 (C= 3.09)
#2	Secondary	872.00'	<b>12.0' long x 1.0' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31 3.30 3.31 3.32
#3	Discarded	869.50'	<b>0.270 in/hr Exfiltration over Surface area</b>

**Post-Development**

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**Discarded OutFlow** Max=0.01 cfs @ 12.25 hrs HW=871.37' (Free Discharge)↑ **3=Exfiltration** (Exfiltration Controls 0.01 cfs)**Primary OutFlow** Max=3.27 cfs @ 12.08 hrs HW=871.14' TW=871.10' (Dynamic Tailwater)↑ **1=Sharp-Crested Vee/Trap Weir** (Weir Controls 3.27 cfs @ 0.86 fps)**Secondary OutFlow** Max=0.00 cfs @ 1.00 hrs HW=869.50' TW=868.50' (Dynamic Tailwater)↑ **2=Broad-Crested Rectangular Weir** ( Controls 0.00 cfs)**Summary for Pond 71P: Infiltration Basin 71P**

Inflow Area = 68,331 sf, 27.58% Impervious, Inflow Depth > 4.32" for 100 yr event  
 Inflow = 7.55 cfs @ 12.07 hrs, Volume= 24,612 cf  
 Outflow = 3.63 cfs @ 12.25 hrs, Volume= 21,592 cf, Atten= 52%, Lag= 10.4 min  
 Discarded = 0.03 cfs @ 12.25 hrs, Volume= 1,109 cf  
 Primary = 3.60 cfs @ 12.25 hrs, Volume= 20,483 cf  
 Secondary = 0.00 cfs @ 1.00 hrs, Volume= 0 cf

Routing by Dyn-Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

Peak Elev= 871.36' @ 12.25 hrs Surf.Area= 4,784 sf Storage= 7,855 cf

Flood Elev= 873.30' Surf.Area= 11,664 sf Storage= 21,023 cf

Plug-Flow detention time= 106.9 min calculated for 21,582 cf (88% of inflow)

Center-of-Mass det. time= 52.3 min ( 861.7 - 809.4 )

Volume	Invert	Avail.Storage	Storage Description
#1	868.50'	21,023 cf	<b>Custom Stage Data (Prismatic)</b> Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
868.50	0	0	0
869.00	1,015	254	254
869.50	2,765	945	1,199
870.00	3,166	1,483	2,682
871.00	4,010	3,588	6,270
872.00	6,156	5,083	11,353
873.00	7,450	6,803	18,156
873.30	11,664	2,867	21,023

Device	Routing	Invert	Outlet Devices
#1	Primary	862.20'	<b>12.0" Round Culvert</b> L= 69.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 862.20' / 858.00' S= 0.0609 1' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#2	Device 1	869.80'	<b>30.0 deg x 1.30' rise Sharp-Crested Vee/Trap Weir X 2.00</b> Cv= 2.61 (C= 3.26)
#3	Device 1	871.60'	<b>1.2" x 7.3" Horiz. Orifice/Grate X 3.00 columns</b> X 11 rows C= 0.600 in 25.7" x 25.7" Grate (44% open area) Limited to weir flow at low heads
#4	Secondary	871.60'	<b>170.5 deg x 5.0' long x 1.00' rise Sharp-Crested Vee/Trap Weir</b>

**Post-Development**



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
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Cv= 2.46 (C= 3.08)  
 #5 Discarded 868.50' **0.270 in/hr Exfiltration over Surface area**

**Discarded OutFlow** Max=0.03 cfs @ 12.25 hrs HW=871.36' (Free Discharge)

**5=Exfiltration** (Exfiltration Controls 0.03 cfs)
**Primary OutFlow** Max=3.60 cfs @ 12.25 hrs HW=871.36' TW=0.00' (Dynamic Tailwater)

**1=Culvert** (Passes 3.60 cfs of 11.13 cfs potential flow)


**2=Sharp-Crested Vee/Trap Weir** (Orifice Controls 3.60 cfs @ 3.98 fps)


**3=Orifice/Grate** ( Controls 0.00 cfs)
**Secondary OutFlow** Max=0.00 cfs @ 1.00 hrs HW=868.50' TW=0.00' (Dynamic Tailwater)

**4=Sharp-Crested Vee/Trap Weir** ( Controls 0.00 cfs)
**Summary for Pond 72P: Stiles Lake**

Inflow Area = 475,249 sf, 9.11% Impervious, Inflow Depth > 3.51" for 100 yr event  
 Inflow = 34.23 cfs @ 12.18 hrs, Volume= 139,119 cf  
 Primary = 34.23 cfs @ 12.18 hrs, Volume= 139,119 cf, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

**Summary for Pond 73P: DMH7**


Inflow Area = 43,070 sf, 43.75% Impervious, Inflow Depth > 4.69" for 100 yr event  
 Inflow = 5.44 cfs @ 12.07 hrs, Volume= 16,826 cf  
 Outflow = 5.44 cfs @ 12.07 hrs, Volume= 16,826 cf, Atten= 0%, Lag= 0.0 min  
 Primary = 5.44 cfs @ 12.07 hrs, Volume= 16,826 cf

Routing by Dyn-Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

Peak Elev= 873.09' @ 12.07 hrs

Flood Elev= 874.50'

Device	Routing	Invert	Outlet Devices
#1	Primary	871.10'	<b>15.0" Round Culvert</b> L= 9.6' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 871.10' / 871.00' S= 0.0104 '/ Cc= 0.900 n= 0.012, Flow Area= 1.23 sf

**Primary OutFlow** Max=5.43 cfs @ 12.07 hrs HW=873.08' TW=871.13' (Dynamic Tailwater)

**1=Culvert** (Inlet Controls 5.43 cfs @ 4.43 fps)



# GRAZ Engineering, L.L.C.

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March 5, 2019

## Oak Bluff Lane Definitive Subdivision Mounding Analysis for Revised Pond #71P

The following mounding analysis is based on the equations set forth in the “Simplified Solutions for Groundwater Mounding Under Stormwater Infiltration Facilities” by Kaveh Zomorodi (2005).

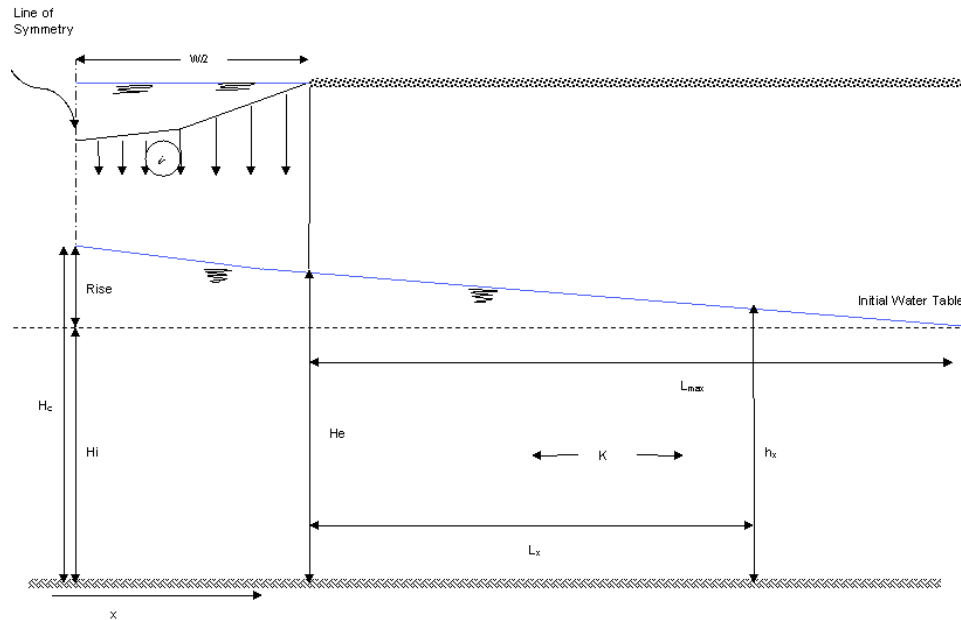


Figure 1. General Layout and Configuration of Mounding under Recharge Strip (Zomorodi, 2005)

The parameters for the mounding analysis are as follows:

$H_c - H_i$  = maximum mound rise at centerline of trench, (ft)

$i$  = average recharge rate in the facility, (ft/day)

$W$  = infiltration basin width, (ft)

$K$  = horizontal saturated hydraulic conductivity of the saturated layer, (ft/day)

$H_e$  = maximum saturated thickness at the edge of channel, (ft)

$L_x$  = any arbitrary distance from the channel edge, (ft)

$L_{max}$  = maximum distance of influence of the mound beyond which mound rise is negligible, ((ft)

$h_x$  = thickness of saturation layer at distance  $L_x$ , (ft)

The parameters for the proposed drainage infiltration basin are as follows:

$i$  = 0.02 ft/day (see calculation below)

$W$  = ±16 ft

$K$  = 0.72 ft/day (see attached NRCS Web Soil Survey data, 2.55 micrometers per second)

Calculations for  $i$ :

$R_{avg}$  = average rainfall in Leicester = 48 inches (Worcester, MA)

$V_1$  = system storage volume for 1 inch rainfall depth = 147 ft<sup>3</sup>

$A_{bt}$  = bottom surface area of infiltration basin (Sand Bottom Elev. 863.7) = 967 ft<sup>2</sup>

$$\text{Therefore: } i = \frac{147 \text{ ft}^3}{967 \text{ ft}^2} \times \frac{48 \text{ storms}}{\text{year}} = 0.02 \text{ ft/day}$$

967 ft<sup>2</sup>      year      365 days

Equation 3 for Mound Rise at center of Trench (Zomorodi, 2005)

$$(H_c - H_i) = \frac{0.86 (i) (W)}{(K - i)} = \frac{0.86 (0.02) (16.0)}{(0.72 - 0.02)} = \underline{\underline{0.4 \text{ ft}}}$$

Equation for Maximum Lateral Distance Extent (Zomorodi, 2005)

$$L_{\max} = \frac{1.72 (K) (W)}{(K - i)} - \frac{W}{4(K)} = \frac{1.72 (0.72) (16.0)}{(0.72 - 0.02)} - \frac{16.0}{4(0.72)} = \underline{\underline{22.8 \text{ ft}}}$$

Based on the above calculations, the predicted groundwater mound rise under the centerline of the proposed infiltration basin (Pond #71P) is 0.4 ft. The high side of the basin bottom has been set at existing grade (869.5). The separation between the bottom of the proposed infiltration basin and the estimated high groundwater table at this location is approximately 2.8 feet (TP-71P, ESHGWT = 34"). Therefore with the predicted groundwater mound rise, there will be ±2.4 feet of separation between the bottom of the basin at the high side of the basin and the high point of the groundwater mound rise.

In addition, the maximum lateral distance extent of 22.8 feet would be within the outer shoulder of the infiltration basin access drive which has a design elevation of 873.3 feet so there would be no issue with breakout and bank erosion due to the minimal mounding effects of the proposed infiltration basin.

Should you have any other questions or require additional information prior to the meeting please call me as soon as possible.

Respectfully yours,  
GRAZ Engineering, L.L.C.

  
Brian MacEwen, P.L.S., E.I.T.  
Project Manager

  
Paul Grasewicz, P.E., P.L.S.

BCM/PFG/bcm

cc:      Matt Schold, Central Land Development Corp.  
         Paul Grasewicz, GRAZ Engineering, LLC

**Site Recharge to Groundwater****"Static Method"**

Soil type: **C**  
 Impervious Area (A1): **42,408** s.f.

Rawls Rate: **0.27** In./Hr.

Soil type: **D**  
 Impervious Area (A2): **13,114** s.f.

Hydrologic Group	Target Depth Factor (F)	
A	0.60	inches
B	0.35	inches
C	0.25	inches
D	0.1	inches

**Determine the required recharge volume:**

$R_v = F \times \text{impervious area}$

$R_v$  = Required Recharge Volume

$F$  = Target Depth Factor

$$R_v = \frac{F \text{ "HSGC" } \times A1}{12 \text{ in. / ft.}} + \frac{F \text{ "HSGD" } \times A2}{12 \text{ in. / ft.}} = \mathbf{993 \text{ Cu.Ft.}}$$

**From Hydrocad determine the elevation that will hold back the required recharge volume:**

Below is a excerpt from the stage storage table of Infiltration Pond 71P.

Required Site  $R_v = \mathbf{993}$  Cu.Ft., the minimum low level outlet required = **869.39**

Stage Storage Volumes				
Elevation (Ft.)	Surface Area (Sq.Ft.)	Inc. Storage (Cu. Ft.)	Cum. Storage (Cu. Ft.)	
868.5	0	0	0	
869	1,015	254	254	869.39 El. At $R_v$ Min.
869.5	2,765	945	1,199	
870	3,166	1,483	2,682	2385 $R_v$ at LLO
871	4,010	3,588	6,270	
872	6,156	5,083	11,353	
873	7,450	6,803	18,156	
873.3	11,664	2,867	21,023	

The Low Level Outlet (LLO) has been designed at elevation: **869.80**

**Determine if the infiltration BMP will drain completely within 72 hours:**

$$\text{Time drawdown} = \frac{R_v}{(K) (\text{Bottom Area})}$$

$R_v$  = Storage Volume at Low Level Outlet (LLO) Elevation

$K$  = Saturated Hydraulic Conductivity (Rawls Rate)

Bottom area = Bottom surface area not including sidewall

$$\text{Time drawdown} = \frac{2,385}{\frac{0.27}{12 \text{ in. / ft.}} \times 2,571} = \mathbf{41 \text{ hours}}$$

**Result is satisfactory for design purposes**

**41 hrs. < 72 hrs.**